

TABLE XLIV. FATIGUE STRENGTHS OF HIGH-STRENGTH STEELS FROM PUSH-PULL TESTS AT ELEVATED TEMPERATURES^(a)

| Material | Test Temp., F | Ultimate Tensile Strength, ksi | Yield Tensile Strength, ksi | Test Conditions ^(c) | α_r , Stress Range Parameter ^(b) , for Cycles | | | |
|---------------|------------------|-----------------------------------|--------------------------------|---|--|-----------------|-----------------|-----------------|
| | | | | | 10 ⁴ | 10 ⁵ | 10 ⁶ | 10 ⁷ |
| D6AC | 450 | 260 | 175 | $\begin{cases} \alpha_m = 0 \\ \alpha_m = \alpha_r \end{cases}$ | 0.56 ^(d) | 0.48 | 0.40 | 0.31 |
| | | | | | 0.41 | 0.35 | 0.31 | 0.26 |
| D6AC | 550 | 230 | 160 | $\begin{cases} \alpha_m = 0 \\ \alpha_m = \alpha_r \end{cases}$ | 0.65 | 0.52 | 0.41 | 0.33 |
| | | | | | 0.44 | 0.38 | 0.34 | 0.29 |
| Vascojet 1000 | 800 | 260 | 200 | $\begin{cases} \alpha_m = 0 \\ \alpha_m = \alpha_r \end{cases}$ | 0.69 | 0.56 | 0.42 | 0.31 |
| | | | | | | 0.40 | 0.32 | 0.23 |
| Vascojet 1000 | 1000 | 230 | 176 | $\begin{cases} \alpha_m = 0 \\ \alpha_m = \alpha_r \end{cases}$ | 0.75 ^(d) | 0.61 | 0.43 | 0.26 |
| | | | | | | 0.39 | 0.27 | 0.21 |

(a) Data are taken from Reference (39).

(b) $\alpha_r \equiv (\sigma)_r / \sigma_u$, $\alpha_m \equiv (\sigma)_m / \sigma_u$, where $(\sigma)_r$, $(\sigma)_m$, σ_u are the semirange, mean, and ultimate tensile stresses, respectively, at temperature.

(c) The cycle rate was 3100 cps.

(d) S-N curve extrapolated to 10⁴ cycles.

The fatigue data available are only for positive and zero mean stresses. However, there is evidence that compressive mean stress may significantly increase the fatigue strength^(35,40). The reasons for this are thought to be that compression may reduce the detrimental effect of fluid pressure entering minute cracks or voids in the material and the compression may restrain such flaws from growing. Since the liner of a high-pressure container can be precompressed by shrink-fit assembly, an important factor in triaxial fatigue may be the prestress that can be initially provided. Therefore, for 10^4 to 10^5 cycles triaxial fatigue life, α_r and α_m are assumed to be

$$\alpha_r = 0.5, \alpha_m = -0.5 \quad (11a, b)$$

as indicated in Figure 42. With $\alpha_m = -\alpha_r$ the maximum tensile stress at the bore would be zero.

In order to approximate a life of one cycle, it is assumed that

$$\alpha_r = 1.0, \alpha_m = 0, \text{ for one cycle} \quad (12a, b)$$

which represents a cycle between $\pm\sigma_u$, the ultimate strength.